行政院國家科學委員會專題研究計畫成果報告

殖民建築的文化想像:以淡水埔頂地區為例

The Cultural Imagination of Colonial Architecture in Pu-ding District, Tan-shwei

計畫編號:NSC 88-22 1-E-032-012

執行期限: 87/08/01 ~ 88/07/31

主持人:米復國 淡江大學建築系副教授

一、中文摘要

淡水是外國勢力進駐後如何進行空間 計畫的一個重要的觀察點,尤其是埔頂 埔頂地區的空間變遷,歷經三百年間各時 期不同的變化,它是在一個地區中, 勢力進駐淡水、洋人居留區的劃定、 勢力進駐淡水、洋人居留區的劃定、領事 館的設立、洋行資本的入侵、教會力 维動,以及住宅、醫館、學校的興築,本 地買辦紳商的仿造。

關鍵詞:殖民建築、後殖民、文化想像、 淡水、埔頂

Abstract

Tan-shwei is an important viewpoint of observing how foreign influence affects a place and its space program. Within Tanshwei, the Pu-ding area has its specially interesting space changes because of its three-hundred-long exposure under different ethnic

changeover. For example, the entrance of foreign forces, the designation of residence for them, the establishment of consulates, the institution of foreign firms, the promotion of churches, the construction of residences, hospitals, and schools, and local compradors' imitation of these new foreign concepts, all contributed to its space changes.

This research observes the landscape of Tan-shwei, especially that of Pu-ding. At the angle of cultural imagination, we try to find how and why, historically, the western culture changed this space. By examining the changes in the form and the function of the colonial architecture in Pu-ding, we can see the cultural impact in different periods and the indigene's response and imagination to that. Thus, we choose this certain area and try to hit the mark in space by exploring the literature, poetry, paintings, and figures in different times, in order to discuss the cultural imagination and the consequent cultural identity in the colonial architecture and place.

Keywords: Colonial Architecture, Tan-shwei, Post-Colonial, Cultural Imagination

二、計畫緣由與目的

文化想像基本上是預設了資本全球化 是殖民主義的延伸,要理解/解構當代文化 的型構一主體的構成,就需回到殖民史特 定時/空操作所帶來的效果,而效果內容與 形成是特定地理空間在既有的歷史型構與 殖民史相互碰撞的結果。因此它指涉的地 理空間不僅是前殖民地,也是帝國基地。 在掌握特定地理空間將殖民史的重構所形成的文化造型,經過比較研究,就較能精 確描繪當代的文化想像的地圖。

本研究選定淡水埔頂的地景與相關文 本作為研究的主題,主要的目的有:

1. 瞭解淡水埔頂歷史發展與地景變遷的關係:將焦點集中在分析殖民者與被殖民者關係背後的社會意識,這樣的社會意識如何展現在地景的塑造上。不在描述整段埔頂的空間發展,而是從發展的歷史中抽出在變遷的過程中影響各不同立場的族群進行分析,瞭解文化的想像如何及為何對淡水及埔頂空間進行改造的行為。

三、結果與討論

(一)、淡水埔頂地景變遷

1. 西荷時期埔頂聖多明哥城的興建是在險峻,有防禦工事及可遠眺的觀測點上,可看到通風衛生問題及西洋工程技術與防禦的想像。在整個北台灣發展可看到當時西班牙人的據點以社寮島為重心,沿路廣大海岸擴展,西班牙在雞籠和平島建立聖薩爾瓦多城為主要的發展地點,聖多明哥城成為西班牙拓展疆域的邊緣。

個空間是作為軍事的要地,更重要的是作 為官方的用地,成為漢人的移民者無法任 意接近的空間領域,將市街發展的方向與 油車口散村的聚落切斷了。

4. 日治時期的埔頂主要有淡水中學與 淡水女學校的發展,從變遷分析中可看到 新一批傳教士在此地的努力以及日本人如 何進行同化行動的改正過程,主要的地景 改變集中在學校建築與宿舍上。

5. 戰後埔頂的地景發展成為歷史建築物的使用,包括古蹟的指定與歷史建築物的再利用,其次是軍眷宿舍及現代營建技術的建築,包括別墅、服務高爾夫球場建築設施、學校內的教堂、高層集合住宅、軍眷宿舍的出現成為在時代交替下社會空間轉換的具體例證。

(二)、淡水埔頂殖民建築樣式的分析

英國領事館官邸代表著一種西方殖民國家 到異地產生的社會關係模式,沿襲著早期 的渡假、第二個家的概念,變化成辦公管 理與家居混合、研究的地方,而這個案例 移植到漢人的世界中,轉化成了一種表徵 地位、財富、社會聲望的象徵,包括了紅 樓與白樓的興建背後所彰顯的意識形態。

3. 從馬偕教堂的類型演變中以及文本的描述裡,共同性來自禮拜的文化層次,並以漢人熟悉的事物附會進去,以博得與此認同的基礎。馬偕以象徵的意像在專漢人的意像來抵抗外來的象徵意義,出現了強烈的衝突局面。從這裡可以看到馬偕本身對如何將傳教打入漢人社會所產生的認同焦慮。

(三)、各時期文化想像:

2. 清代郁永河的文本中看到了漢人對 異文化的想像,除了社會風情、自然風物 的描述外,也有文人對時政的批判,其特 殊性在於他的作品不只流於自我心情的寄 託,更有社會關懷的取向,就官方的角色 而言是以清人統治者的角色來觀察台灣, 就中國文人而言,文本的寫作表現出紀遊 、紀實的風格,背後隱藏著官方以方志來 了解地域特色的想像,以遂行統治的策略 ,他所描述的是關乎記憶再現的過程,也 就是記憶選擇的操弄過程,異地特俗的紀 實寫作隱藏在中國人如何看到淡水的差異 地景。而清代描述淡水意象的文人除了用 中國意象的景色、山川、人物來類比於淡 水的地景特色,並進行個人的感遇舒懷, 中國才是他心中的故鄉。對地方平民而言 日常生活中是由一些當地地景的特徵描述 來傳述統治的意像,而這樣的關係是更直 接深化到平民的生活中,其使用的名詞亦 各異,但一致的是形成一種「塑造世界」 的力量。

益與宗教的分野中有其彈性。而漢人對異 教信仰的迫害,顯露出人性晦暗的一面。

4. 日治時期一些異俗攝影與明信片的 流行展現出殖民時期的影像情境,散佈到 大眾媒體,並且製造了真實的假象,同時 這樣的行為打破混雜著學術與知識訊息的 傳遞,如同觀光商品一樣被操縱或哄抬之 下的產物。攝影與旅遊的發達,配合日本 人破除地方化空間,旅遊的行為成為探點 式的攫取地方文化的想像,同時異國風味 的影像形成一種隱喻性的經驗,出現在風 景名勝的觀光用書或寫真帖。旅遊的行為 成為探點式的攫取地方文化的想像,隱含 著因日本帝國建設使這些地方方被整頓得 讓眾人能一覽無遺。這種現象在柯設偕的 淡水文本裡出現了浪漫的異國情調、混同 了世界各地域類似的意象,淡水在柯設偕 的想像裡深化了日本內化傾向,以一種中 性且富想像的形容詞來描述,這樣的論述 與敘述與清代官書的寫法是極為不同的, 在社會意義上也相異於統治階級。這烏托 邦的想像又附著於他本身特殊的身世、信 仰。同時他把過去淡水歷史遺留的事蹟、 空間以大眾媒體介紹到社會上,期待眾人 對這淡水空間進行鄉愁的眷戀。西川滿的 文本融匯民俗、宗教、歷史的研究,對淡 水的想像包括了對歷史原始史料的添加與 改寫、揉合了歷史典故及正史的傳聞,混 同著西川滿本身信仰特殊的紛圍。以具體 的物象不斷的聯想,將日治時期新的事物 融入他的詩中,將歷史建築本身空間及物 件的空間意象予以轉化並故事化,以增添 傳奇的色彩,漢人傳統的束縛變成他採樣 鄉野傳奇的故事題材。

5. 戰後以「紅毛城事件」為主題的李雙澤、李立國等相關文本可見到七〇年代紅毛城在民間成為反對帝國主義的想像圖騰,在這背後是官方將台灣社會文化加區,在這背後是官方將台灣社會文化加工。 鄉土化方不致危及權力集團內部中國國現代史」「傳統對現代」的提法形成了「傳統對現代」的提法形成了「傳統中國」對「現代中國」與「鄉土」、「專根」、「民間」及「寫實」的主題或形式接合 。但作為現實生活世界裡的人們以及諸多現代小說詩作的文本,雖然跨越了時間的限制,鮮明將現實的記憶與過去發生的事蹟連結,以「記憶的鍊金術」混同各種文化,揭示了文化錯置的淡水,也出現了敘事者的焦慮及拒絕被定位的企圖。

四、計畫結果自評

雖然只是一個小的地區,但跨越的時間卻有三百多年(西、荷、明鄭、清、日治、戰後),加上各種外來勢力交織,使得本研究變得異常複雜。在有限的時間下,只處理了各歷史時期的文化想像。以致於有關當代(前)的討論力有未逮,這是對後殖民論述的一個疏失。

本研究的成果主要有:

- 1. 淡水埔頂地景各時期歷史發展與 地景變遷的分析。
- 2. 淡水埔頂殖民建築的處境與社會 作用的分析。
- 3. 淡水埔頂殖民與去殖民文本的文 化想像與地景變遷背後意識形態關連性 的分析。

五、主要参考文獻

1. Ashcroft, Bill, Gareth Griffiths, and Helen Tiffin. (ed.) (1995) The Post-Colonial Studies Reader. London and New York: Routledge. 2. Nalbantoglu, G.B. and C.T. Wong (ed) (1997) Postcolonial Space(s). New York: Princeton Architecture Press.

- 3. Said, Edward. (1993) <u>Culture and Imperialism</u>. New York: Vintage.
- 4. Williams, Patrick and Laura Chrisman (ed.) (1993) Colonial Discourse and Post-Colonial Theory. London: Harvester Wheatsheaf.

 5. 張京媛編, (1995) 《後殖民主義理論與
- 文化認同》台北:麥田出版有限公司。 6. 米復國,(1997) 《1860s-1890s 淡水、大 稻程、艋舺殖民建築研究:殖民與後殖民
- 8. 陳光興, (1996)<去殖民的文化研究> (台灣社會研究季刊) 21:73-139。

論述考察》淡江大學建築研究所。

$$\frac{di_{\alpha s}}{dt} = -\left(\frac{R_s}{L_{\sigma}} + \frac{R_r L_m^2}{L_r^2 L_{\sigma}}\right)_{i_{\alpha s}} + \omega_e i_{\beta s} + \frac{R_r L_m}{L_r^2 L_{\sigma}} \psi_{\alpha r} + \frac{\omega_r L_m^2}{L_r^2 L_{\sigma}} \psi_{\beta r} + \frac{1}{L_{\sigma}} \omega_{\alpha s} \quad s(t) = x(t) - \int_0^t (a+bk)x(\tau)d\tau = 0 \tag{7}$$
where k is a linear feedback gain to be designed.

$$\frac{di_{\beta s}}{dt} = -\left(\frac{R_s}{L_{\sigma}} + \frac{R_r L_m^2}{L_r^2 L_{\sigma}}\right)_{i_{\beta s}} - \omega_e i_{\alpha s} - \frac{R_r L_m}{L_r^2 L_{\sigma}} \psi_{\alpha r} + \frac{\omega_r L_m^2}{L_r^2 L_{\sigma}} \psi_{\beta r} + \frac{1}{L_{\sigma}} \omega_{\beta s} \tag{8}$$
When the sliding motion occurs, $s(t) = \dot{s}(t) = 0$, the dynamical behavior of the controlled system

$$\frac{d\psi_{\alpha r}}{dt} = -\frac{R_r}{L_r}\psi_{\alpha r} + \frac{R_r L_m}{L_r L_\sigma}i_{\alpha s}$$

$$T_e = \frac{3 P L_m}{2 2 L_r} \psi_{\alpha r} i_{\beta s}$$

The associated mechanical equation can be described as

$$J\frac{d\omega_m}{dt} + B\omega_m + T_L = K_t i_{\beta s}$$
 (2)

where K, is defined as the torque constant.

$$K_{t} = \frac{3}{2} \frac{P}{2} \frac{L_{m}}{L_{r}} \psi_{\alpha r} \tag{3}$$

Furthermore, one should the mechanical equation (2) with uncertainties

$$\frac{d\omega_m}{dt} = (a + \Delta a)\omega_m + (b + \Delta b)i_{\beta s} + dT_L \tag{4}$$

One further defines the speed error as

$$x(t) = \omega_m(t) - \omega_m^{\bullet} \tag{5}$$

where ω_m^* is the speed command. Taking the derivative of (5) with respect to time yields

$$\frac{dx}{dt} = ax(t) + b[u_{\beta s}(t) + e(t)]$$
 (6)

where

$$u_{\beta s}(t) = i_{\beta s}(t) + \frac{a}{b}\omega_m^*$$

and

$$e(t) = \frac{\Delta a}{b} \omega_m(t) + \frac{\Delta b}{b} i_{\beta s} + \frac{d}{b} T_L$$

According to the redefined uncertain system (6). the sliding surface with integral component is designed as follows:

$$s(t) = x(t) - \int_0^t (a + bk)x(\tau)d\tau = 0$$
 (7)

where k is a linear feedback gain to be designed. is equivalent to

$$\frac{d}{dt}x(t) = (a+bk)x(t) \tag{8}$$

From (8) it is evident that, in the sliding mode, the speed error x(t) will asymptotically converge to zero without being affected by the perturbation. That is the controlled rotor speed ω_m can track the desired speed command ω_m^* asymptotically.

To assure the existence of the sliding mode. the following assumption is firstly given

$$|e(t)| < \beta$$

i.e., the lumped perturbation e(t) has an upper bound β . Then, based on the uncertain system (6) and the designed sliding surface (7), the

$$u_{\beta s}(t) = kx(t) - \beta \operatorname{sgn}(s(t))$$

variable structure speed controller is designed as where sgn(.) is a sign function defined by

$$\operatorname{sgn}(s(t)) = \begin{cases} 1 & \text{if } s(t) > 0 \\ -1 & \text{if } s(t) < 0 \end{cases}$$

The above sliding mode controller design is based on an ideal indirect field-oriented control. However, it is known that both rotor time constant and mutual inductance are uncertain. In this case, the estimated slip speed will deviate from actual value. As a result, the decoupled property of the field oriented control will lost.

Self-Decoupling Method Using Short **Duration Pulses**

To get an ideal indirect field-oriented control, this section proposes an on-line tuning method for estimating the slip gain. The method is by superimposing short duration rectangular pulses Δi_{cc} on the flux command current i_{cc} . Observing the dynamical equation of the rotor flux ψ , in terms of the flux producing current.

It can be seen that the rotor time constant governs the changing rate of rotor flux. Accordingly, if the given flux command pulses are short relative to the rotor time constant, the rotor flux magnitude will not change significantly. Figure 1 shows the rotor flux magnitude resulting from a short rectangular pulse of flux command. It shows a small decrease in rotor flux, approximately -5\%, during the flux command pulse.

Under perfect operating conditions, the parameters of the vector controller are matched to those of the induction machine, giving a slip calculation without error. This assures that the actual synchronous rotating frame matches the estimated frame. Thus, the rectangular pulse in the flux command current will not affect the controlled speed. However, if the stator current vector i_s is projected on the actual synchronous rotating frame (α and β axis) and on the estimated frame ($\hat{\alpha}$ and $\hat{\beta}$ axis). It can be seen that if the estimated slip gain \hat{K}_s is less than the actual value K_s , the calculated slip speed $\hat{\omega}_s$ is less than the actual slip speed ω_s , since the slip speed is proportional to the slip gain K_s . In this case, the actual synchronous rotating frame moves ahead of the estimated frame. If one superimposes a rectangular pulse Δi^*_{∞} on the flux command current i^*_{∞} based on the estimated $\hat{\alpha}$ -axis. Therefore, the rectangular pulse $\Delta i^*_{\alpha s}$ can be decomposed into two components, Δi_{cs} and Δi_{fs} , based on the actual synchronous rotating frame,. The component Δi_{cx} does not affect actual flux component much; however, component Δi_{Bs} will increase the developed torque.

Based on the above analysis, one sees that a

short rectangular pulse Δi^*_{cc} superimposed on the flux command, according to the estimated $\hat{\alpha}$ - $\hat{\beta}$ frame will change the actual developed torque, which is related to whether the estimated slip gain \hat{K}_s is less, the same or greater than the actual slip gain K_s . As a result, the speed controller will produce a torque command current to compensate the change of the developed torque due to the flux pulse. To assure the overall system robustness, a variable structure speed controller is combined with the proposed slip gain estimating method. Figure 5 shows the torque command current produced by the variable structure speed controller for three cases of the estimated slip gain value. It can be seen that the polarity of the torque change gives an indication of whether the estimated slip gain \hat{K}_s is less, the same or greater than the actual slip gain K_{s} .

Accordingly, based on the change of the torque command current, the following algorithm is used to adjust the estimated slip gain \hat{K}_s .

- Step 1: Sample the torque command current $i_{\beta c(k)}^*$ at two points:
 - (a) The first point is at the start of the flux pulse and is assigned to be $i_{R(k)}^*$.
 - (b) The second point is at the end of the flux pulse and is defined to be $i_{\beta s2(k)}^*$.

Step 2: Substitute $i_{\beta s_1(k)}^*$ and $i_{\beta s_2(k)}^*$ into

$$\hat{K}_{s(k+1)} = K_{p} (i_{\beta s l(k)}^{*} - i_{\beta s 2(k)}^{*}) + \hat{K}_{s(k)}$$

Step 3: Repeat from Step 1 at the start of the next flux pulse command.

IV. Experimental Results

The experimental results of a 800 W induction motor are used to test the proposed variable structure speed control with self-

decoupling algorithm. The convergence of the estimation algorithm of the slip gain is verified by experiment results shown in Figures 2 and 3. Figures 2 and 3 show the tuning of the slip gain under operating the motor speed at 150 rpm with $T_L = 1.0 \text{ N-m}$, and the initial gains set at $\hat{K}_s(0)=1.9$ and $\hat{K}_s(0)=7.6$, respectively. It can be seen that estimations converge to the same value.

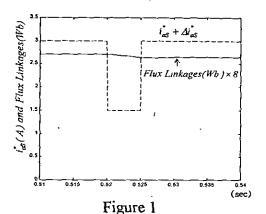
Conclusions

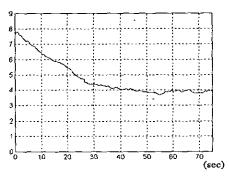
In this study, a new self-decoupling method by estimating the slip gain in the computation of the slip speed for indirect fieldoriented control is proposed. The decoupling method is combined with a novel variable structure controller with integral sliding surface for the speed control of the induction motor drive. The estimating method applies a short duration pulse on the flux command current. The slip gain is then tuned according to the variations on the torque command current from the variable structure speed controller. With the slip estimation algorithm, the indirect fieldoriented controlled induction motor drive is robust to the deviation of the slip gain to get a decoupled field-oriented control. Moreover, due to the property of the special design of the integral sliding surface, the acceleration signal needed in the conventional variable structure speed controller is removed. The novel variable structure speed controller also provides the robustness for disturbance load. Finally, experimental results are provided to verify the validity.

References

- [1] Seung, K.S., "A novel technique of rotor resistance estimation considering variation of mutual inductance," IEEE Trans. Ind. Appl., 1989, vol. 25, no. 4, pp. 578-587.
- [2] Wade, S., Dunnigan, M.W., and Williams, B.W.,"A new method of rotor resistance

- stimulation for vector-controlled induction machines," IEEE Trans. Ind. Elec., 1997, vol. 44, no. 25, pp. 247-257.
- [3] Hung, J.Y., W. Gao and J. C. Hung, "Variable structure control: A survey," IEEE Trans. Ind. Electron., vol. 40, no. 1, pp. 2-22, 1993.
- [4] E. Y. Y. Ho and P. C. Sen, "Control dynamics of speed drive systems using sliding mode controllers with integral compensation," IEEE Trans. Ind. Applicat., vol. 27, no. 5, pp. 883-892, 1991.
- [5] Shyu, K.K., and Shieh, H.J., "A new switching surface sliding-mode speed control for induction motor drive systems," IEEE Trans. Power Elec., 1996, vol. 11, no. 4, pp. 660-667





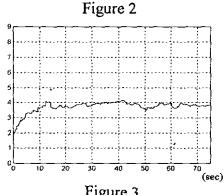


Figure 3